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The NIST Digitally Synthesized Power Calibration Source

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NATIONAL INSTITUTE OF STANDARDS & TECHNOLOGY Research Information Center Gaithersburg, MD 20899

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THE NIST DIGITALLY SYNTHESIZED POWER CALIBRATION SOURCE

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A digitally synthesized source of "phantom" power for calibrating electrical power and energy meters is described. Independent sources of voltage, current, and phase angle are programmable between 0-240 volts, 0-5 amperes, and 0-360 degrees, respectively. The uncertainty of the active and reactive power is estimated to be within ± 100 ppm of the full scale apparent power (volt-amperes).

Key Words: calibration, digital waveform synthesis, power measurement, TDM wattmeter, transconductance amplifier, voltage amplifier, wattmeter, watt-hour meter.

1. INTRODUCTION

Calibration of wattmeters and watthour meters has traditionally been made by comparing the meter under test (MUT) to a standard wattmeter or watthour meter. The advantage of that approach is that ^a precise knowledge of the source parameters is not required. Voltage and current amplitudes and the phase angle between them need only be known approximately and the stability of each of these parameters is not critical as long as the power or energy output of the MUT is averaged or integrated over the identical period as that of the standard instrument. With the advent of multifunction instruments capable of measuring voltage, current, power factor, and active and reactive power, a knowledge of each of the source parameters has become advantageous. The measurement of reactive power and energy, in particular, is greatly simplified if the source of voltage, current, and phase angle is known and stable.

This approach has led to the development of a dual-channel sinewave source of voltage and current, which is shown in figure 1. Previous experience with digital waveform synthesis methods [1-6] provided the basis for designing a precision digital waveform generator to synthesize two low-level sinusoidal signals, which are programmable in both amplitude and phase angle. An illustration of ^a 20-step digitally synthesized signal, and the sine wave from which the sampled points were derived, is given in figure 2. A special voltage amplifier A1 [7] was designed to scale the low-level voltage $V₁$ to typical test levels ranging from 60-240 V, while test currents ranging from 1-5 A are obtained with ^a specially designed transconductance amplifier A2 [8]. The source is controlled by ^a desk-top computer that is linked to auxiliary instrumentation for measuring the analog and digital outputs of the MUT .^{1}

¹ In order to describe adequately the systems and tests discussed in this report, commercial equipment and instruments are identified by manufacturer's name and/or model number. In no case does such identification imply recommendation or endorsement by the National Institute of Standards and Technology, nor does it imply that the material or equipment identified is necessarily the best available for the purpose.

The controller for the power calibration source is a Hewlett Packard 9836 desk-top computer equipped with one megabyte of memory, ^a general purpose input/output (GPIO) interface card, and ^a DMA card. Data is transmitted and received at the generator rear panel through the 50-line GPIO cable (see HP 98622A GPIO Interface Installation manual for pin connections).

Figure 1. Block diagram of the power calibration source. Figure 2. A digitally synthesized

waveform.

2. HARDWARE

2.1 Digital Generator

The heart of the power calibration source is a digital generator (see fig. 3), which synthesizes voltages V_1 and V_2 in a staircase or "zero-order-hold" approximation to a sinusoidal waveform. Two signals whose waveforms are independently programmable are constructed by sequentially applying digital values stored in random access memories, RAMI and RAM2 to 18-bit multiplying digital-to-analog converters, MDACl and MDAC2. The values stored in memory are equally spaced samples of this waveform with up to 2048 discrete steps per period. For normal operation the stored functions are sinewaves; however, any arbitrary waveforms with up to 1024 harmonic components may be stored. The phase angle between the two waveforms is determined by changing the set of function values stored in RAM2.

The theoretical resolution of the phase angle separating a pair of digitally synthesized sinewaves is a function of the resolution of the processor used to calculate the sample points, the resolution of the generating DACs (this determines to what extent each step is quantized), and the number of steps (sample points) per period. The algorithm used to calculate the sample points is performed with adequate precision in the computer to introduce negligible errors. The generating MDACs, capable of 18-bit precision, are normally used as 16-bit converters to speed up data transmission. These MDACs may be updated at $1 \mu s$ intervals, and at 60 Hz, 2048 steps are used to synthesize one period. The angular resolution under these conditions (based on computer simulations) is approximately one microradian [9].

The amplitudes of V_1 and V_2 may be set independently between 0-10 volts-peak by controlling the dc reference voltages supplied to MDACl and MDAC2 with ^a second pair of 18-bit DACs. This technique provides an amplitude resolution of approximately 38 μ V (10/2¹⁸ volts). The offsets of all four DACs may be adjusted remotely over a range of ± 500 ppm by employing four additional 8-bit DACs. This technique provides a means for trimming the dc offset and gain of each of the generated waveforms that is adjustable under software control.

Figure 3. Block diagram of the dual-channel digital generator.

The frequency of the generated waveforms is a function of the number of steps per period and the sample rate (for a 60 Hz sine wave with 2048 steps the sample rate is 122.88 kHz). A programmable frequency synthesizer is used to generate the clock signal, which provides the strobe pulse for each sample point. It has a short-term stability of approximately 1 part in 10^8 .

A detailed description of the digital generator hardware is given below, Note that figure 3 is a simplified diagram that does not include some of the hardware discussed below.

2.1.1 Optical Isolator

Data from the HP GPIO passes through the Optical Isolator Board (fig. 4) to separate the generator ground from the computer ground. Since the generator is ^a "listener," only the GPIO output lines and the handshake signal lines PCTL, PFLG, and CTLO are optically isolated. The HP 2630 (Ul-U8, U12) optical isolators invert the data, which is restored to the correct polarity with inverting buffers (U9-U11). The PFLG, which originates at the generator (and is the only outgoing line), is isolated separately in U13. The 5-volt power supply used to terminate the GPIO lines is ^a Datel dc-dc converter mounted on the board.

2.1.2 Interface

Once isolated, the data is decoded in the Interface Board (fig. 5). The GPIO data is separated into ^a "data" bus and ^a "control" bus which steers the data to the appropriate board. Whenever the GPIO data is changed, the PCTL line is pulled high (about $1 \mu s$ after the data is valid). Data is latched into U1 and U2 by this PCTL line when CTLO is high. When CTLO goes low, the output buffers U6-U9 are enabled, placing the control word on edge connector pins 3-18.

The PFLG, which is normally low, is pulsed high for $1 \mu s$ (time set by R1 and one-shot U4), about l/is (set by R2 and CI) after the positive edge of PCTL. This logic provides ^a timed handshake with the GPIO interface, holding the data on the data bus (edge connector pins 38-53) for 1 μ s.

2.1.3 Memories

The sample point values of the generated waveforms are stored in random access memory (RAM) located on the Memory Board (fig. 6). GPIO data is transferred from edge connector pins 21-28 (most

Figure 4. Optical isolator board.

Figure 5. Interface board.

Figure 6. Memory board.

significant 8 bits) and 56-63 (least significant 8 bits) through transceivers U23-U26 to the data lines of the reference channel RAMI (U17,U18) and the variable channel RAM2 (U28,U29). The transfer path and the RAM chip selects are latched into U4 before the data is transmitted, and the RAM write enable signals are derived from the PCTL signal through U12-U14. Addresses for RAMI are generated in the address counter circuit (U1,U2,U5,U6,U7,U15,U20 and U21) which is driven either from PCTL (during loading) or the synthesizer clock (during operation). Similarly, U2,U3,U8,U9,U10,U16,U21 and U22 comprise the address counter for RAM2.

Each memory holds 2048 16-bit words, and the waveforms can be constructed from all or ^a binary fraction of the 2048 data values. The selection of steps is made by programming the appropriate bits into U1, U2 and U3 to increment the address counters by 2^n where n can vary from 0-11.

2.1.4 Digital-to-Analog Converters

The waveforms stored in RAMI and RAM2 are converted to low-level voltage waveforms in the digital-to-analog converter (DAC) Boards - one for each output channel (fig. 7). Data to generate the waveform appears at edge connector pins 40-57 and are latched into U1,U2 (for 16 bits) and U3 (for ¹⁸ bits) by the SYNTH CLK line. Multiplying digital-to-analog converter (MDAC) U8 converts the data word to a corresponding voltage level within a maximum swing of ± 10 volts. U10, an optional buffer amplifier, boosts the output current from ± 10 mA to ± 100 mA.

The output waveform amplitude is adjustable from $0 - 10$ volts-peak by adjusting the dc reference to MDAC U8 (pins $24,25$) between $0 - 10$ volts-dc. The amplitude resolution of MDAC U9 used for this adjustment is 18 bits, and this data is loaded in 8-bit bytes into latches U4,U5,U6 from data on edge connector pins 5-12. The data in these latches is converted to ^a dc voltage in MDAC U9 and amplifier U2. Two edge connections, REF IN and INTERNAL REF, are provided on the board so that an external reference may be used to generate MDAC U9's reference voltage. If no external reference is available, the INTERNAL REF pin must be connected to the REF IN pin.

The dc-offsets for both U8 and U9 are programmable through U11 (a dual 8-bit DAC) and U13 (dual operational amplifiers), which provide dc-offset adjustment of about ± 250 ppm of full scale amplitude. The resistors connected to pins 2 and 6 of U13 convert the unipolar 10-volt outputs to bipolar \pm 5-volt outputs.

2.1.5 Frequency Synthesizer

The system clock pulse, used to control waveform generation by latching new data into each DAC Board, originates in the Frequency Synthesizer Board (fig. 8). This is a composite, two-piece board that uses a commercial frequency synthesizer (Syntest model SM-102 with 5½ digit resolution) and a decoder/latch board, which holds the 5-BCD digits and the 3-bit frequency range data. The data is held in latches U1,U2 and U3, which are enabled for loading by U4. The Syntest board has been modified (voltage regulators removed) so that it will operate with $+5$ V and $+15$ V power supplies instead of the original $+5$ V and +24 V supplies.

2.1.6 Power Supply and Rear Panel Wiring

The generator requires one 5-volt, 5-ampere power supply for the digital circuitry and one ± 15 volt, 1-ampere power supply for the analog circuitry. These supplies are connected to the analog and digital hardware through an Amphenol connector as shown in figure 9. Pin connections for the rear panel GPIO connectors are also shown in this figure. The 50-pin connector attaches to the controller, while the 24 pin IEEE-488 type connector provides optically isolated GPIO-data to the SWITCH BOX (described in 2.4) and other peripheral devices as needed.

Figure 7. DAC board.

Figure 8. Frequency synthesizer board.

Figure 9. Rear panel GPIO connections and power supply connector.

2.1.7 Board Location and Back Plane

The generator consists of six boards, occupying slots 1,2,3,5,7,9 (see fig. 10) of a commercial card cage made by Cambion. The back plane wiring diagram for this card cage is shown in figure 11.

Figure 10. Cambion cardcage slots showing generator board locations.

Figure 11. Generator back plane wiring.

2.2 Voltage Amplifier

2.2.1 Circuit Description

The voltage amplifer (described in detail in [7]) was primarily designed to boost the output amplitude of the digital generator in order to provide the nominal 120 or 240 rms voltage output of the power calibration source. This amplifier has a fixed gain of 40 and can provide a maximum output voltage swing of ⁹⁷⁰ volts peak-to-peak or ³⁴⁰ V rms at ¹⁰⁰ mA rms. The bandwidth is from dc to ¹⁵⁰ kHz and at 60 Hz the observed no-load, short-term amplitude and phase instabilities are ± 5 ppm and ± 5 microradians, respectively. The amplifier design uses high voltage N-channel MOSFETs in the output driver stage together with a unique circuit topology of opto-isolators between the low-level input stage and the highlevel output stage. In addition, the amplifier was designed to supply up to ¹⁰⁰ mA rms to accommodate the burden requirements of electrodynamic type meters without causing significant error. A prime goal was to maintain the excellent short-term amplitude and phase stability inherent in the digital generator.

Figure 12a shows the circuit diagram of the voltage amplifier. Each polarity output driver uses a pair of ¹⁰⁰⁰ V, N-channel MOSFETs to provide ^a 2000 V capability to each polarity driver. The stacked pair of MOSFET drivers provides an operating voltage safety factor of two for each device when operating at maximum peak-to-peak output signal swing. In addition, the total power dissipation for each driver pair is equally divided between two devices. A small trimmer capacitor C23, helps to balance the differential capacitance across the opto-isolator pair U3 so that the high frequency response for the positive and negative output signal can be better matched. Diodes CR3 & CR4 separate the signal at the output of U2 and steer the respective polarities to each driver. U2 is ^a high gain wideband operational type amplifier that provides the major portion of the open-loop gain for the voltage amplifier. U2's input offset errors are reduced by the gain of Ul, which in effect servos out any offset errors at the summing junction. In order for this scheme to be effective, Ul must be ^a precision low-offset type of amplifier. A local compensating network (C1,R7) around U2 is necessary in order to shape the gain-bandwidth response to avoid loop oscillation. The diodes at the summing junction protect the amplifiers U1 $\&$ U2 against high voltages during turn-on and output voltage slew-rate limiting.

Figure 12b shows the voltage amplifier's monitoring, control, and overload protection circuitry. U4 converts the amplifier's ac output to a dc value corresponding to the output rms amplitude, while the low pass network (R20, R21, C11, C12) and diodes CR1, CR2 enable relatively small dc output offsets to be monitored in the presence of large ac output signals. Switch SW2 selects which of these signals is to be displayed by the front panel meter. Power to the output stage is controlled by relay K3, K2, and K1, switch SWl, and the state of flip-flop Ul. U3 serves as ^a bipolar peak detector that toggles Ul when ^a preset output current is reached, which in turn removes the power to the output drivers. The output stage will remain shut down until Ul is reset by Switch SWl.

Figure 12a. Complete circuit diagram of precision voltage amplifier: Amplifier circuit.

Figure 12b. Complete circuit diagram of the precision voltage amplifier: Control and overload protection circuitry.

 $\overline{\mathcal{D}}$

2.3 Transconductance Amplifier

2.3.1 Circuit Description

A complete circuit diagram of the transconductance amplifier (described in detail in [8]) is shown in figure 13. The operation of the circuit can be described as follows: A voltage applied to the main input at F, produces a current into a load connected across the output terminals. The load current causes a voltage drop across R20 which is amplified by a factor of 10 by a differential amplifier circuit composed of U5 and resistors R16 through R19. The output of voltage the differential amplifier is fed back via R21, where it is compared with the input voltage at the summing junction of U2. Thus, the output current is made proportional to the input voltage. Within the output compliance voltage range, the transconductance amplifier will maintain the same output current for a fixed input voltage regardless of any load change. Since the differential amplifier circuit that senses the voltage across R20 is part of the feedback loop, its phase lag creates a potential source of instability for which compensation must be added. Compensation is provided by modifying the loop-gain response to have a single dominant pole by means of a capacitor C7 across R21.

Figure 13. Complete circuit diagram of the transconductance amplifier.

The output power booster stage, consisting of Ql through Q4, is ^a class AB complementarysymmetry emitter follower designed to provide an output current of approximately 15 amperes. Amplifiers U3, U4, and transistors Q5, Q6 provide complementary fixed current sources for the output booster stage. The output stage is designed to have a quiescent operating current of about 250 mA, which keeps crossover distortion to an acceptable level. Practical considerations for achieving stable operation require proper highfrequency power supply bypassing with both electrolytic and ceramic capacitors at each collector of the booster stage. Also, careful attention must be given to circuit grounding and load ground returns.

2.4 Switch Box

The main purpose of the switch box is to facilitate the automation of watt/watthour meter calibration and system test procedures. The switch box is also used for source monitoring. A complete schematic of the switch box circuitry is given in figure 14. The switch box contains switching and control circuitry which enables up to 6 meters under test, MUT1-MUT5 and ^a non-standard MUT, to be calibrated conveniently. For each of the first ⁵ meters, MUT1-MUT5, there are two switch box inputs provided, one for the MUT's analog current output and one for the MUT's pulse output, which is assumed to be configured as ^a standard TTL, open-collector. The non-standard MUT is provided with only one analog voltage input. The relays in the box are remotely programmed over ^a portion of the HP GPIO bus that has been channeled through the digital generator. These bus output pins are located on card cage slot 2 pins 11-28 and exit the digital generator via a rear panel IEEE-488 type connector (see fig. 9).

2.4.1 Circuit Description/Programming

The triangular, numbered tabs in figure 14 represent wiring traces present on the actual circuit board of the switch box. The traces were represented this way for the sake of schematic clarity. Connections to and from the switch box, measuring devices, and MUTs are made at the circles labeled "R" and "B", for "red" and "black" banana plugs, as well as at other connectors labeled in the figure. The analog outputs of each standard wattmeter are connected to the switch box inputs as shown in figure 14. For energy measurements, each MUT's open-collector pulse output is first "pulled up" to $+5V$ before being channeled through multiplexer U6 to the switch box's counter output. The frequency of the pulse output may be measured by any frequency counter capable of being connected to the controller via an IEEE-488 bus.

For power measurements, the circuit includes an array of both latching and non-latching relays. The relays are switched using either line drivers, (U1,U4), or latches, (U2,U3). The non-latching relays (Sl-SIO) are switched using the buffered outputs of latches Ul and U4. These relays are used to switch the current output of a selected MUT from a low-precision 1-k Ω resistor to the standard 1-k Ω resistor used in an actual power measurement. The latching relays (R1-R6) require only ^a brief pulse from line drivers U2 and U3. This pulse is provided by programming U5, a 3-8 line decoder, to toggle output pin #15 low by toggling pins 4,5 with the generator's CTLO signal (control bus enable). These latching relays (R1-R6) channel the voltage outputs of various devices to the system DVM input. These voltages include the generator's dc-offsets, the output of the non-standard MUT, the Guildline 1300A Transfer Standard's output (used in the Power Bridge [10]), the transconductance amplifier's monitor output, and the voltage amplifier's output. With the ability to automatically sample these signals using the system DVM and counter, power and energy measurements can be made simultaneously in intervals of ten seconds per MUT.

The generator's control/data bus is also used for programming the switch box (for programming codes, see sec. 3.5.4, table 2). The programming steps are similar to those required to program the generator's internal boards. These steps are performed in the subprogram. Switch, as described in section 3.4.4.

Figure 14. Complete circuit diagram of the switch box.

³ SOFTWARE

3.1 The MET_6 Program

There are three basic functions performed by the MET 6 software. First, to control the digital generator, second, to characterize and correct generator errors so that they fall within certain bounds, and third, to semi-automate wattmeter testing procedures. The latter tasks are performed by a group of routines that are very system dependent and may be omitted with only minor changes to the basic software. The MET 6 program was written initially in HP BASIC version 2.1 for use on an HP 9836C desktop computer. With the required binary drivers, the program will also run on HP BASIC 3.0 and 5.0 on HP series 200 and series 300 machines (equipped with the series 200 keyboard).

3.2 Software Considerations Based on System Configuration

3.2.1 Switch Box vs. no Switch Box

There are several MET 6 variables that must be properly defined, depending on whether the power/energy calibration system includes a switch box (as described in sec. 2.4) or not. Certain subprograms use these variables to determine the proper measurement algorithm to follow (see sec. 3.4). Table ¹below lists these variables and their values based on system configuration. For a complete explanation of all variables used in the MET 6 program, see APPENDIX A.

To set the variables listed above in table 1, the procedure is as follows:

- 1. "PAUSE" the program and "EDIT" the line # given;
- 2. Change the value in the indicated line and "ENTER" it;
- 3. "RE-STORE" the program (or, "PURGE" and "STORE").

3.3 Generator Control Routines

Figure 15 outlines the relationships between the various routines and is intended to show only their basic interactions, not the detailed program execution flow. These routines may be separated into two groups consistent with their relative utility. The first to be discussed, the interactive I/O group, share a common symmetry of operation that allows them to be easily understood and maintained. These are the Adj_phase, Synth_load, Amplitude, and Cor_dac subprograms. The rest of the subprograms may be loosely grouped together, based on the fact that they perform specialized tasks that require little or no interaction with the user.

Figure 15. Basic relationships of various routines in the MET_6 program.

In the discussion below, the term 'function key' refers to the ten rectangular keys labelled kO through k9 found on all HP series 200 desktop computers. Two lines at the bottom of the computer's screen indicate the alphanumeric labels assigned to each k0-k9 key. For clarity, the labels that appear on

the computer screen during the MET_6 program execution are enclosed in quotes in the discussion below. Also, numbers, shown in brackets refer to the length of ^a string, not to the references at the end of this report.

3.3.1 Interactive I/O Routines

3.3.1.1 Amplitude

To enter this routine, press the "AMP." function key when in the main menu. Three additional choices will appear - "REF_WAVE", "VAR_WAVE", or "EXIT". The first two choices are for reference waveform and variable waveform amplitude control, respectively, while the third will cause an exit to the main menu. Pushing the "REF WAVE" function key will cause four additional keys to appear - "AMP", "GAIN", "OFFSET", AND "LINEAR". In order to enter₁ the Amplitude subroutine, press the "AMP" function key. Once inside the subroutine, there are three ways in which the user may alter the amplitude value: 1) pressing the ± 100 to ± 1 least significant bit (LSB) function keys, 2) turning the keyboard knob, or 3) directly entering the desired value. The three columns located on the lower portion of the screen indicate the amplitude, change from the initial value in LSB's, and the apparent and actual amplitude DAC settings, respectively. On the screen, the binary string under the "APPARENT" heading is the DAC amplitude setting corresponding to the amplitude value on the lower left of the screen, while the binary string under the "ACTUAL" heading includes any gain corrections that may be present.

Gain, dc offset, and amplitude linearity corrections are handled by the routine Cor_dac (see sec. 3.3.1.3 below). Since the amplitude values Ref amp and Var amp are used within the software in many calculations, including gain corrections, the Amplitude routine should only be used to set up the ideal (desired) amplitude. The Amplitude routine automatically calls Cor_dac after every amplitude change, resulting in a constantly updated dc offset voltage correction corresponding to a linear correction curve. In addition. Amplitude routine computes a new gain correction according to a similar correction curve set up in Cor_dac. After ^a call to Amplitude routine, the internal variables Ppm and Voltage (see app. A) are corrected to values allowable by the 18-bit amplitude DAC (U9 on the output board). A discussion of how to characterize the generator and construct these curves is given in section 5.

Due to software gain DAC corrections, which are transparent to the user, the Amplitude routine behaves rather unpredictably when incrementing the amplitude DAC near full scale, which is the amplitude where the voltage amplifier is automatically enabled. The DAC settings on the lower right of the screen were included mainly as a way of keeping track of exactly what is happening during this discontinuity of operation.

If, when the keyboard knob is used to increment the gain or amplitude, a value is selected that exceeds the maximum output DAC binary setting, the user will be alerted to this fact and the output DAC set to its maximum value.

Finally, provisions are made in the Amplitude routine to remotely enable or disable the voltage amplifier with the (kO) function key. Enabling or disabling is accomplished by entering the Amplitude routine via the "REF AMP" key and then using the "ENABLE" (k0) function key. The amplifier is automatically enabled when the operator enters ^a reference voltage above 7.071 V (full scale of amplitude DAC for sinewave functions).

3.3.1.2 Adj phase

To enter this routine from the main menu, use either the "PHASE" or "OFFSET" function key. To set up ^a direct reading phase difference between the reference and variable waveform channels, first use

the "OFFSET" key to adjust the inherent channel phase error to zero and then use the "PHASE" key to set the desired phase difference. The phase difference between the two channels is computed as the difference between the global variables Phaz and Offst. For example, the effective phase difference between the two waveforms resulting from a Phaz of 30 degrees and an Offst of ¹ degree is 29 degrees.

The behavior of the I/O subroutines in Adj_phase is similar to that of Amplitude, Cor_dac, and Synth load. The main difference between Adj phase and the others is that the actual output of the new waveform values and address difference is done in another subprogram, Change phase, which is described in section 3.3.2.

Adj phase has two modes of operation, fine and coarse. In the coarse mode, only the RAM address difference is changed, resulting in a phase resolution of 1/2048. In the fine mode, although the algorithm used to compute the values in RAM allows for an extremely fine resolution, ^a reasonable value for the highest resolution was chosen to be 1 μ rad. When changing the phase at intervals lower than 1/2048, Adj_phase calls Change_phase with Sel_ect=2 ($1=$ coarse, 2=fine) and also passes the real arrays Real_var and Var diff to Change phase, where it recalculates the integer buffer values and outputs them to RAM.

3.3.1.3 Cor_dac

This subprogram may be accessed from the main menu by pressing the "AMP." function key, choosing either "REF_AMP" or "VAR_AMP," and then deciding whether Cor_dac is to process "GAIN," "OFFSET," or "LINEARITY." In each of the three cases, the operation of Cor_dac is as follows:

(a) "GAIN" key ($k3$ or $k8$): The functionality of the routine is similar to that of the Amplitude subprogram (see discussion above in sec. 3.3.1.1). The values across the lower portion of the screen represent the gain correction in volts presently being applied to the Ref amp or Var_amp variables, the change (in ppm of reading) between the desired voltage (Ref_amp or Var_amp) and the corrected voltage, and the "APPARENT/ACTUAL" DAG settings, respectively. The routine uses the input parameters Slope, Intercept, and Voltage to calculate Ppm and then calls Amplitude (see fig. 15) to load the new corrected amplitude DAC word into the appropriate generator output board. An additional function performed by the call to the Amplitude routine is to return to Cor dac a corrected value of Ppm, since only discrete values are permitted by the 18-bit DAC. In the gain mode, Cor dac does not directly manipulate Ppm. Instead, Slope is altered and Ppm recalculated.

(b) "OFFSET" key (k4 or k9): Operation is similar to "GAIN" above. Cor_dac controls the amplitude DAC's offset voltage by altering the setting of the 8-bit MDAC (U11 on the output board). To do this, Cor dac must be called with the input parameter, Dac choice, set to 1. In the offset mode, Cor_dac uses the input parameters Slope, Voltage, and Intercept to calculate an 8-bit value, Vo_lts, that is then loaded into U11 of the appropriate output board. In this mode, Cor dac does not manipulate Vo Its directly. Instead, it increments or decrements Intercept. This seems to be the best method because the characteristic slope of the dc offset correction curve seems to stay relatively constant over time. The values displayed across the lower portion of the screen are from left to right the applied DAC setting in volts and the change (in LSB's) between the present 8-bit DAC setting and the initial setting (shown ai the top of the screen).

(c) "LINEARITY" key (k2 or k7): In this mode, Cor_dac controls the A-channel of the 8-bit dual MDAC (Ull) on the appropriate output board. The behavior of Cor_dac in this mode is similar to that discussed in the above "OFFSET" mode with the exception that Cor_dac manipulates Voltage directly with no reference to either of the input parameters Slope or Intercept. The purpose of this routine is to ensure that the amplitude errors are constant (the same ppm of reading) throughout the voltage range.

A discussion of how this is accomplished is given in the section on generator characterization. Once this value is determined, it should not be changed until the next output board adjustment, or else serious amplitude non-linearity may result.

$3.3.1.4$ Synth load

This is the controller subprogram for the generator's frequency synthesizer board. To enter this routine from the main menu, simply press the "FREQ." function key (k7). The methods of data input are identical to the Amplitude, Adj phase, and Cor dac routines, which are direct entry, knob turning, or choosing a defined function key.

Because of the synthesizer's design, the actual value of an LSB in Hz is highly dependent on which frequency range the synthesizer board is presently set on. In the event of a frequency change, the Synth load routine determines both the proper range and frequency resolution of the synthesizer board's output, the latter of which may range from as fine as 10μ Hz to as coarse as 100 Hz.

The internal structure of the subprogram is very straightforward. Since there are no frequency corrections, the Synth load routine basically performs only two tasks: 1) to handle user I/O, and 2) to update F, the variable containing the current frequency synthesizer setting. The Synth load routine contains only one input parameter, Freq, that is usually passed by value. The seemingly redundant presence of both F and Freq stems from the fact that Freq does not always indicate the true synthesizer setting. For instance, when Freq = 10,000 (10.000 kHz), F = 10.000 and F unit $\mathbf{S} = \text{H}$ KHz." Calling Synth load with Freq $= 0$, an illegal value for the synthesizer board (see data sheet), causes the subprogram to initialize its I/O handling subroutines, Format and Softkey. Thus, Synth_load may be used to simply set up a synth board setting or to also interact with the user.

3.3.2 Subprograms to Perform Specific Generator Control Tasks

3.3.2.1 Change_phase

This is a subprogram invoked by Adj_phase that performs the actual generator channel phase changes. Depending on the value of Sel_ect, Change_phase will either calculate the address offset between the two channels and call Cnt_vals to output this value to the memory board (Sel_ect=1) or Change_phase will use matrix operations to calculate new variable channel RAM values and then call Out put to load the new values and set the address offset (Sel ect=2). This process can be more clearly understood by examining fig. 15.

3.3.2.2 Cnt_vals

This subprogram is transparent to the user and is responsible for loading the memory board's RAM address counter with the desired increment in order to create a phase difference between the two channels. The desired increment is passed (usually by value) to Cnt vals via the input parameter, Address add. The variables L2_mss and L2_lss, which correspond to latch U2 on the memory board, are updated during each call to Cnt vals.

3.3.2.3 Init

This subprogram initializes the appropriate channel's Real and Diff arrays as well as the integer buffer used to output the values to RAM. Depending on the parameter Functions, Init will calculate 2048 sin, ramp, triangle, square, zeroes, ones, minus ones, or arbitrary function values, load the values into the Real, Diff, and BUFFER data structures, output the BUFFER to the appropriate memory(s), and finally, reset the correct amplitude values on the output boards.

3.3.2.4 Out_put

This is a subprogram responsible for loading the appropriate memory channel(s) with the contents of the INTEGER buffer passed to it. Out put also takes care of restoring the proper counter increment (RAM address offset) by calling Cnt vals.

3.3.2.5 Process_key

This is a subprogram designed to eliminate the use of the Basic "INPUT" command, which halts program execution and disables the function key interrupt routines when waiting for an "ENTER" command. Process key acts upon a keyboard interrupt and checks the keyboard buffer. The subprogram then interprets the data as either legal or not, depending on the Message input parameter. Upon the occurrence of an "ENTER" key, Process key then either returns the accumulated data in Value (numeric input only) or shifts it into Value\$ (alpha-numeric data). Process_key may also update Message according to the data passed to it (see the code documentation).

3.3.2.6 Set inc

This subprogram sets up the memory address counter according to the variable Inc, the number of steps per period. The desired increment is stored in another variable, Inc_rement, because Inc must be set to zero during certain memory board operations.

3.3.2.7 Status

This subprogram is usually called after the completion of an interactive I/O subprogram. Status displays the following parameters: Fr_eq, F*Inc, Inc, Rivd, Civd, Offst, Phaz, Ref_amp, Var_amp, R_funcS, and V func\$.

3.3.2.8 Step_num

This is a subroutine that allows for the manipulation of the number of steps per period of the output waveform. The default value of 2048 may be decreased in binary steps down to ^a minimum of ² steps per period by using either the defined function keys or by direct entry. The basic steps taken to accomplish this are: 1) call Set_inc to set the proper memory board counter increment 2) call Synth_load to set the new sampling rate 3) recalculate the rms value of the waveform, and 4) restore the proper phase value by calling Change phase.

3.3.2.9 Wav_gen

This subroutine handles the I/O tasks for the subprogram Init (see 3.3.2.3 above). The type of waveform to be loaded in memory as well as the desired channel, may be chosen by using the defined function keys.

In order to load ^a specific arbitrary waveform, the program must first be "PAUSE"d and line 4100 of Init modified. To preserve this function as the arbitrary waveform the program containing this updated line 4100 must be "RE-STORE"d.

3.3.2.10 Machine_state

This subprogram may be accessed from the main menu by using the "MORE" (k0) key and then the "GEN VALS" (k4) key.

The purpose of this routine is to allow the user to either store or retrieve all major generator variables from disk storage. These groups of variables (generator states) are contained in the files "Gen state," the file reserved for temporary state storage, and "Met6vals," the file reserved for permanent (default) state storage, resident on the MET 6 program disk.

Once inside the Machine state subprogram via the "GEN VALS" key, the three resulting choices are "EXIT" (k0), "DEFAULT" (k4), and "TEMP" (k9). "DEFAULT" is used to retrieve/store values from "Met6vals" while "TEMP" operates on "Gen_state." To store the present state as the default state, use the "DEFAULT" and then "STORE" function keys. To retrieve the generator's default state from disk, use the "DEFAULT" and "RETRIEVE" keys. The same procedure applies when using the "TEMP" function key.

The "GEN VALS" key may also be used to save calibration system configurations for several different test points by setting up the system at the desired point, inserting a disk dedicated for power/energy calibrations at this test point and "STORE"-ing the system state in the "TEMP"-orary state file. In this way, system setup data as well as error data for specific test points may be collected on separate disks (see sec. 3.4.1 below for information concerning calibration error data storage).

3.4 Generator Characterization Subprograms

The subprograms in this section are ones which aid in characterizing the digital generator. Once the correction factors are determined, these routines may also be used to fine tune the corrections or to adjust the correction for a different operating point. The discussion presented here deals mainly with how the routines function and with gaining an understanding of how to use them. Section 5. discusses in detail how an actual characterization of the generator is carried out using these routines.

3.4.1 Calibrate

This routine employs a rotating menu system that gathers relevant input parameters for use in the subprogram. Measure. To enter this subprogram from the main menu, press the "MORE" (k0) and then the "CALIBRATE" (k5) function keys. From this point, there should be three function key options, "SELECT> OPTION," "SECOND PAGE" or "EXIT." In addition, the user may move around the menu by using the keyboard knob.

The menu used in Calibrate contains two levels. The first page, or primary menu, contains the choices between which generator characteristics are to be measured. Pressing the "SECOND PAGE" function key (k9) will result in the relevant Measure input parameters to be displayed in a similar (secondary) menu. These parameters relate to the row at which the arrow was pointing prior to entering the secondary menu by pressing the "SECOND PAGE" function key. In order to verify this, the top line of the screen in the secondary menu should be the same as the selected row in the primary menu. To return to the primary menu, press the "FIRST PAGE" key (k9) that has replaced the "SECOND PAGE" key.

The various input parameters for both the Calibrate and Measure subprograms are stored in string, integer, and real array structures, which are named Calib val $\{(12,4)$ [30], Cal int vals $(10,5)$, and Cal r vals(10,6), respectively. These values are stored in the ASCII file "CAL_VALS" and are loaded during program initialization. The "CAL_VALS" file may be created by running the program Calval_config in the PROG file "C_VAL_CON."

It is sometimes necessary to alter the values stored in the above data structures. To do this, the user must be in the secondary menu. Once there, the keyboard knob is used to point to the desired parameter, which will be highlighted in blue, if the monitor is color, or white, if the monitor is

monochromatic. The new value may then be "ENTER"ed through the keyboard. If the value is a valid one,it should appear in the red (color monitor) or white (monochrome monitor) field after hitting the "ENTER" key.

The measurement cycle must be started in the primary menu, so to get there, use the "FIRST PAGE" key and then the "SELECT> OPTION" (k0) key. At this point Calibrate will turn control over to the Measure subprogram. If ^a data disk with the proper filename is not present in drive "INTERNAL," the subprogram Measure will pause and wait for either the file to be created or the disk to be put in the drive. To find out the filename, press "filenameS" and "EXECUTE." If at any time ^a filename other than the default name is desired, a different one may be set by performing the following steps:

- 1. Leave the ":INTERNAL" drive empty before using the "SELECT>OPTION" key.
- 2. Wait for Measure to pause.
- 3. "EXECUTE" a command like "Filename\$=xxx."
- 4. Reinsert the disk with the filename on it.
- 5. "CONTINUE" the program.

3.4.2 Compliance

This subprogram is used to add an extra gain term to the variable channel waveform in order to correct for transconductance amplifier gain changes when operating at different output compliance voltages. Compliance first calls Measure to measure the ac compliance voltage across the output of the transconductance amplifier. This value is them used in a linear correction equation involving C_slope and C intercept to evaluate C ppm, which is then added (in ppm of reading) to all subsequent variable channel amplitude DAC settings. The procedure for characterizing the generator for compliance related amplitude errors is given in section 5.3.

To enter Compliance from the main menu, press the "AMP.", "VAR_WAVE" and "COMPLIANCE" softkeys in that order. When entering Compliance, there are only two choices, to "EXIT" or to "READ COMPLIANC." Before enabling the " $+10$ PPM" or " $+1$ PPM" function keys, the current amplifier's compliance voltage must first be read. After that, these keys may be used to increase or decrease the intercept of the compliance correction curve, C intercept.

To ensure the proper variable channel gain correction is present, Compliance should be used whenever the burden on the transconductance amplifier changes.

3.4.3 Measure

Subprogram Measure is used to take automated measurements using either a Hamburger K2004, HP 3456A HP 3457, or FLUKE 8506A. Measure may be used to take either single data points returned in the input parameter. Value, or it can take groups of data in which some generator parameter (usually amplitude) has been incremented throughout a range specified in the subprogram. Calibrate.

If the variable Row > 0 upon entry to Measure, the routine uses the contents of Calib val $(12,4)$ [30], Cal int vals(10,5), and Cal r vals(10,6) assigned in Calibrate (see discussion above) to control its remaining execution path. The various fields of these data structures are assigned in the following way:

In the above list, the expression " (x,x) ," where "x" stands for any allowable array index or the index given, represents the two-dimensional index for the listed data structures. For an explanation of these variables, see the table of MET_6 variables, APPENDIX A.

When subprogram Measure is called with variable Row \leq 0, the routine takes only a single measurement, returning the value read in Value. The conventions are:

This is a simple, fast subprogram that employs recursion to zero the dc offset of either the reference or variable waveform channel. The code for this routine is very simple, but because it calls Measure, the output of the channel to be zeroed must be connected to the HP 3456A input. IMPORTANT: For the variable channel waveform, the inverting output monitor of the transconductance amplifier must be used or Offset_zero won't behave properly. This routine is called by Measure when Row = 3 or Row = 6 ("V(I)-AMP OFFSET LINEARITY") in the Calibrate subprogram.

3.4.4 Offset zero

Offset_zero may also be reached from the main menu by pressing the "AMP.", "REF_AMP" or "VAR_AMP", "OFFSET" and "ZERO DC OFFSET" function keys in that order.

3.5 Subprograms useful for Power/Energy Calibrations

The subprograms discussed here were developed primarily for the calibration of power related instrumentation using the generator alone or in a power bridge implementation. The purpose of these routines is to automate the testing procedures with the aid of the Switch Box (see sec. 2.4). As mentioned initially, these routines are not necessary for the basic operation of the generator and may be deleted if so desired.

3.5.1 Digit

Because of its relative complexity, this subprogram has been separated into two parts, Digit (the I/O portion) and Body (the measurement and error calculation portion).

To enter Digit, press the "DVM" (kl) function key. The screen is arranged into separate fields containing values that control both the execution flow and error calculations present in Body. Each column contains the complete set of variables required by Body to test the Power/Energy instrument at a single test point. Each row has the following meaning:

The contents of these fields are stored in the arrays Meas_str\$ and Meas_vals in the following way:

For an explanation of the Meas_vals values, see the table of MET_6 variables, APPENDIX A.

The INTEGER array Scr mat $(1:8,1:6)$ serves as storage for indexes to the third dimension of the Meas valS array. These indexes are then utilized by Digit to keep track of what to print in the chosen field and by Body for controlling its execution cycle.

To perform a test using Digit, the various parameters must be set up on the screen. First, enter the serial number of the meter under test (MUT) in row ¹of the column on the screen corresponding to the desired Switch Box channel. Move to this field by using the knob or arrow keys. When using the knob, the highlighted field will move in the direction of the last direction key hit. Once in the appropriate field the channel will not become active until the blinking serial number field is "ENTER"ed. At this point the field should stop blinking and a string of asterisks should appear below the serial number. Continue down the column until all parameters are set appropriately for the specific MUT. When in rows ³ and 4, the values in these fields may be changed by using the "[]" (kO) function key. Repeat this procedure for the remaining meter columns.

Column 6 on the screen is intended for the use of non-standard meters that have voltage rather than current outputs. When performing ^a power/energy measurement with the MUT's information entered in this column on the screen. Digit reads the dc output of the meter, not the value across the standard resistor.

The "DATA STORAGE=" field indicates whether or not the error information printed on the printer is also to be stored on disk (see the "STORE DATA" (k9) softkey explanation below).

Once that all the screen parameters have been set up, push the "MORE" (k9) function key. The behavior of the remaining keys is as follows:

- "RESISTOR CORR" (k3): Digit usually uses a default value of 1 k Ω for the standard resistor value. This routine allows the user to enter the exact value of an available resistor. This value will be used in subsequent error calculations for all the active channels except the non-standard meter under test (NSMUT).
- "DVM CORR" Pressing this key results in two choices, "10 V RANGE COR" $(k1)$ or "1 V RANGE COR" (k6). These represent the error (in Ppm) of the HP 3456A when reading either ¹⁰ V dc or ¹ V dc. Like "RESISTOR COR," these values will be used in subsequent error calculations for all the active channels including the non-standard meter under test (NSMUT).
- "DUMP DATA" Pressing this key results in a catalog of the :INTERNAL,4,1 drive to be displayed along with a prompt asking for the desired filename. The only allowable files are BDAT files; all others will generate an error. The program interprets the contents of the file as ASCII characters and dumps them on the screen, so a file containing data of type

REAL, for instance, will generate garbage on the screen. This key is useful for viewing files containing calibration error data; it will only work, however, when the "DATA STORAGE=" field is enabled.

"STORE DATA" (k9): This key enables or disables the subprogram's data storage option. When enabled, the "DATA STORAGE=" field indicates "YES" and whatever is printed on the printer by the calibration subprogram is also stored as ASCII data in a file named according to the current date. For instance, the filename generated for the first file of Oct 2, 1955 would be "Oct255₁." Successive files for the same date are generated as the data buffer becomes full, i.e., "Oct255_2." This key must be enabled in order to enable an HPIB interrupt service routine within Digit called Send to pc (see discussion below).

Digit may also be configured to send error files to other computers over the IEEE-488 bus. Whenever the "DATA STORAGE=" is enabled, Digit will service an SRQ interrupt using the routine "Sen to pc" and transfer specified files according to various parallel poll and serial poll responses. This routine is not enabled, however, whenever Digit is busy conducting a test.

3.5.2 Guildline

This subprogram is used to measure the ¹²⁰ V rms signal of the voltage amplifier with the Guildline 7100A Thermal Transfer Standard. This subprogram may be reached from the main menu by using the "MORE" (k0) and "7100A" (k1) function keys. The user may select the number of readings to be performed at each of the four settings. The routine will sound a long, low-pitched beep when the setting of the Guildline requires changing. After being switched, the routine allows a settling time of 12 seconds. Once the Guildline has settled, the routine gives a noticeably higher-pitched, shorter beep that indicates it is beginning its measurements. The results of the measurement appear on the screen as ppm of reading based on ^a nominal value of ¹²⁰ V rms.

3.5.3 Ivd

This routine is called from Status where its results are displayed on the screen and stored in the variables Rivd and Civd. These values correspond to the resistive and capacitive inductive divider settings that are required to balance the Power/Energy Bridge at the present phase angle, amplitude values, and frequency.

3.5.4 Switch

This is the switch box controller subprogram. Switch uses two input parameters: 1) Latch, the 8 bit relay data word, and 2) Lat code, the integer value (0-2) that determines which latch is loaded on the switch box. Table 2 is a list of the most frequently used parameter settings $(X = Don't Care)$.

3.6 Miscellaneous MET_6 subprograms

$3.6.1$ Dec to bin

This is a recursive subprogram that converts the input parameter Quotient into a string representation, String\$, of the binary equivalent. Dec_to_bin is mainly used in the Amplitude subprogram, where it is used to display the 18-bit DAC word for amplitude. The main purpose of the routine is for the debugging of control routines. A command that performs this same task is included in some versions of HP BASIC.

3.6.2 Enable

This routine calls Switch to enable or disable the voltage amplifier, depending on the global variable, V_amp.

3.6.3 Print_time

This is a routine used to print the time and date. After using the "MORE" (k0) key in the main function key menu, Print time is called every second to update the time and date located in the upperright of the screen.

To set the time, use the "MORE" and "SET TIME" (k2) keys. Likewise, to set the date, use the "MORE" then "SET DATE" keys.

4. GENERATOR OUTPUT BOARD ADJUSTMENT

Each of the digital generator's two output boards contains two trim pots that must be adjusted (Pot(i) and Pot(ii) on fig. 7). The following steps are required to properly adjust each of the generator's output boards:

(i) Set the amplitude (Ref_amp or Var_amp) to zero. To do this from the main function key menu, use the "AMP." (k8), "REF_WAVE" (k1) or "VAR_WAVE" (k6), and finally "AMP" function keys. Next, exit this routine and enter Cor dac to alter the "LINEARITY" value (see sec. 3.3.1.3). This routine alters the dc offset voltage of the amplitude DAC (U9 on fig. 7). Adjust the 8-bit MDAC until point A is as close to zero as possible. Make sure to note or store this value of $R(V)$ u9 offst using the "STORE" VALUES" (k4) key.

(ii) Set the amplitude to full scale. To do this, enter the Amplitude subprogram and increase the voltage (current) until the "ACTUAL" binary string on the lower left of the screen reads all ones. Now, adjust Pot(i) until point A equals approximately ¹⁰ V dc.

(iii) With the amplitude (Ref amp or Var amp) still set to all ones, enter Wav_gen (see sec. 3.3.3.9) and set the proper memory channel to all zeroes. Now set the dc offset voltage (point B on fig. 7) of the output dac (U8 on Output Board) to zero using Cor dac in the "OFFSET" mode (see sec. 3.3.1.3).

(iv) Finally, with the amplitude still at full scale, use Wav_gen to load all ones into the appropriate memory channel and adjust Pot(ii) until point B equals approximately 10 V dc.

5. GENERATOR CHARACTERIZATION

MET 6 provides for the characterization and correction of the generator's dc offset voltage, waveform amplitude, and the transconductance amplifier compliance voltage errors. Although the subprogram Calibrate is intended mainly for formatting plot data for a plot program, it can also be used for characterizing the generator.

The first step is to adjust the generator's output boards (see sec. 4 above). Second, before performing any runs with Calibrate, all correction terms should be zeroed. This may be accomplished by pausing the program and typing "CALL MACHINE STATE(-1)" and then "EXECUTE."

The remaining procedures for characterizing each of the mentioned parameters are fairly similar and straightforward.

5.1 Dc Offset Voltage

Enter the Calibrate subprogram and choose either the "V-AMP OFFSET LINEARITY" or "I-AMP OFFSET LINEARITY" rows. In the secondary menu, set the parameters to appropriate values if the default ones are incorrect. Connect the output of the desired channel to the DVM and use the "SELECT> OPTION" function key. The Measure subprogram will then call Offset_zero at each test point and store the values $R(V)$ intercept and the applied voltage/current in the chosen ASCII file. NOTE: Offset zero expects the dc offset of the variable channel to be inverted, so either the output monitor of the transconductance amplifier or the inverted sense of the generator's variable channel output must be used. Finally, retrieve these values and perform a linear fit to find $R(V)$ o slope and $R(V)$ o intercept.

5.2 Amplitude

With $R(V)$ slope and $R(V)$ intercept still equal to zero, enter the Calibrate subprogram and use either the "V-AMP INTEGRAL LINEARITY" or "I-AMP INTEGRAL LINEARITY" rows. Both the error (in ppm of full scale) and the nominal voltage are stored in the chosen ASCII file. A linear fit will probably return values for $R(V)$ slope and $R(V)$ intercept that are slightly in error due to the waveform's amplitude errors result in gain correction errors. To avoid the above problem, another method of characterizing the gain is to zero the gain errors at several points, note $R(V)$ intercept at each point and use a linear fit to calculate the proper $R(V)$ slope and $R(V)$ intercept.

5.3 Transconductance Amplifier Compliance Voltage

Since the Calibrate subprogram does not provide a compliance correction mode, the values for C_slope and C_intercept may be found using the following method. First, zero C_slope, C_intercept and Cppm as described above. Now, use the "COMPLIANCE" subprogram (see sec. 3.3.1) at ⁵ A rms to find the proper C intercept for several different transconductance amplifier burden conditions. The resulting linear fit should provide adequate values for C intercept and C slope.

6. SYSTEM PERFORMANCE AND CONCLUSIONS

6.1 System Performance

The power source was originally intended to operate at 60 Hz with 120 V and 5 A sinusoidal waveforms. However, the present source is programmable between 0-240 V and 0-5 A with sinusoidal as well as arbitrary waveforms at frequencies from 0.001 Hz to 100 kHz. These figures represent the limits of amplitude and frequency. Measurements, described in this paper, were performed at 60 Hz and at amplitudes between 20-100% of full scale (FS). The amplitude and phase angle errors given below were obtained by measuring the source using a thermal wattmeter [10] and a current-comparator power-bridge [11].

The amplitudes of the reference and variable channels are changed by adjusting the dc voltages supplied to MDAC1 and MDAC2. However, the output voltages V^1 and V^2 are not ideal linear functions of these dc voltages and thus a gain adjustment is required at different amplitudes. Software gain corrections for any amplitude (based on a linear fit to a few data points) reduce this voltage dependent gain error by a factor of 5-10. Figure 16 shows the residual amplitude nonlinearity, after correction, over a 5 to ¹ amplitude range where 100% of FS represents ²⁴⁰ V and ⁵ A respectively. Differential nonlinearity around 120 volts and 5 amperes is shown in figure 17. The sample points represent a one least-significantbit change (4 ppm of FS) of the respective scaling DACs.

Figure 16. Residual voltage and current integral nonlinearity after gain corrections.

Phase angle accuracy depends upon the initial offset (differential phase shift between channels) and the phase linearity, which is ^a function of quantization errors, DAC nonlinearity, and the number of steps per period. The initial phase offset between the voltage and current waveforms was measured by the current comparator power bridge and adjusted to zero at unity power factor (0°) with an uncertainty of less than 10 microradians.

Subsequent power measurements, with constant voltage and current, between $+90^{\circ}$ and -90° , indicate that the integral phase nonlinearity in this range is less than 20 microradians.

Figure 17. Voltage and current differential nonlinearity around 120 V and 5 A.

Figure 18 shows the differential phase linearity at zero power factor (90°) as measured by a timedivision-multiplier (TDM) wattmeter [12]. This plot not only confirms the computer simulation predictions of ¹ microradian phase resolution of the digital generator, but demonstrates the potential of TDM wattmeters for performing extremely precise measurements around zero power factor as well.

Once the three parameters (voltage, current, and phase angle) have been adjusted and corrected, the major concern becomes stability. Measurements at ¹²⁰ V, ⁵ A over ^a three week period are given in figure 19. The precision of these measurements was approximately 10 ppm in amplitude and 10 microradians in phase. The current drift of 80 ppm has been attributed to aging of the 0.1 ohm shunt in the transconductance amplifier. A simple dc calibration of this amplifier is useful in detecting the gain drift due to the shunt and the results may be applied as an additional gain correction to improve long-term current stability.

Finally, the source was evaluated over a three week period as a power calibrator. Measurements were performed at 120 V and 5 A at a number of phase angles between $\pm 90^\circ$. The source was adjusted at the beginning of the testing period and used to calibrate ^a TDM wattmeter over the next ²⁰ days without further adjustments. Measurements were also performed on the TDM wattmeter using the power bridge, and an envelope which encloses all of the differences between the source and the bridge, using the TDM wattmeter as a transfer standard, is plotted in figure 20. There is a direct correlation between these differences and the current drift from figure 19 as the data for both plots were collected during the same period. If corrected for this drift, the maximum power differences fall within a ± 30 ppm band, as shown in figure 21. These figures include the short-term drift of the TDM wattmeter between the source and bridge calibrations.

Figure 18. Phase differential nonlinearity - generator angle vs change in power indication of a TDM wattmeter at zero power factor.

Figure 19. Long term stability of the source voltage, current, and phase angle as measured by a thermal wattmeter.

Figure 20. Maximun differences between the power calibration source and the power bridge using a TDM wattmeter as ^a transfer standard.

Figure 21. Maximum differences between the power calibration source and the power bridge after correcting for the current drift.

6.2 Conclusions

An accurate and precise source of synthetic power for calibrating watt/watthour and var/varhour meters at the 100 ppm level has been described. The source consists of ^a dual-channel digital waveform generator followed by direct-coupled high-voltage and transconductance amplifiers to provide signal levels of 60-240 V and 1-5 A at any phase angle. Control is provided by ^a desk-top computer and auxiliary instrumentation supports the calibration of up to six test instruments. The uncertainties of source parameters at power frequencies are:

- 1. voltage <30 ppm of FS.
- 2. current <50 ppm of FS (requires ^a periodic monitor of the current amplifier gain).
- 3. phase <20 microradians at FS voltage and current (degrades slightly at lower amplitudes).
- 4. Power (active and reactive) < 100 ppm of FS volt-amperes.

While the source is normally operated under sinusoidal conditions, future applications will utilize its ability to synthesize arbitrary waveforms with dc components. A direct coupled system permits calibration of gain factors at dc where, in general, the resolution and accuracy of measuring instrumentation is greater. Extrapolating results at dc to power frequencies is reasonable and offers the possibility of a calculable ac source based on dc measurements. Furthermore, experience with a direct-coupled system has focused attention on the ever present ground loops that always seem to evolve in a system. In fact, monitoring and eliminating dc offsets created by ground loops has turned out to be a good technique for assuring that ground loops do not create measurement errors which might otherwise go undetected.

7. REFERENCES

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APPENDIX A: Table of Met_6 Variables

$NIST$ Technical Publications

Periodical

Journal of Research of the National Institute of Standards and Technology—Reports NIST research and development in those disciplines of the physical and engineering sciences in which the Institute is active. These include physics, chemistry, engineering, mathematics, and computer sciences. Papers cover a broad range of subjects, with major emphasis on measurement methodology and the basic technology underlying standardization. Also included from time to time are survey articles on topics closely related to the Institute's technical and scientific programs. Issued six times a year.

NonperiodicaIs

Monographs—Major contributions to the technical literature on various subjects related to the Institute's scientific and technical activities.

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