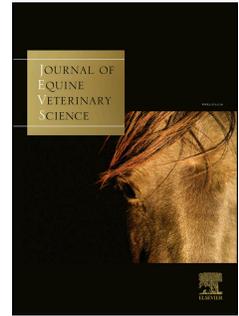


Accepted Manuscript

Equation for Predicting the Load-Pulling Capacity of Traction Equids

Tobias Maia de Albuquerque Mariz, Pierre Barnabé Escodro, Emerson de Lima, Samuel Albuquerque, Carolyn Batista Lima, Jéssyka Emmanuely Silva dos Santos, Andrezza Caroline Aragão da Silva



PII: S0737-0806(18)30084-4

DOI: [10.1016/j.jevs.2018.06.014](https://doi.org/10.1016/j.jevs.2018.06.014)

Reference: YJEVS 2554

To appear in: *Journal of Equine Veterinary Science*

Received Date: 14 February 2018

Revised Date: 29 June 2018

Accepted Date: 29 June 2018

Please cite this article as: de Albuquerque Mariz TM, Escodro PB, de Lima E, Albuquerque S, Lima CB, dos Santos JES, da Silva ACA, Equation for Predicting the Load-Pulling Capacity of Traction Equids, *Journal of Equine Veterinary Science* (2018), doi: 10.1016/j.jevs.2018.06.014.

This is a PDF file of an unedited manuscript that has been accepted for publication. As a service to our customers we are providing this early version of the manuscript. The manuscript will undergo copyediting, typesetting, and review of the resulting proof before it is published in its final form. Please note that during the production process errors may be discovered which could affect the content, and all legal disclaimers that apply to the journal pertain.

1 **Equation for Predicting the Load-Pulling Capacity of Traction Equids**

2

3 Tobyas Maia de Albuquerque Mariz^a, Pierre Barnabé Escodro^b, Emerson de Lima^c, Samuel
4 Albuquerque^c, Carolyny Batista Lima^a, Jéssyka Emmanuely Silva dos Santos^a, Andrezza
5 Caroline Aragão da Silva^b

6 **Affiliations**

7 a- Department of Animal Science, Federal University of Alagoas, Arapiraca, Alagoas state,
8 Brazil, 57309-005. E-mail addresses: tobyasmariz@hotmail.com/ cblzte@hotmail.com
9 /jessyka_emmanuely@hotmail.com.

10 b- Department of Veterinary Medicine, Federal University of Alagoas, Viçosa, Brazil,
11 57700-000. E-mail addresses: pierre.escodro@vicos.ufal.br /
12 andrezzaaragaovet@hotmail.com.

13 c- Institute of Physics, Federal University of Alagoas, Arapiraca, Brazil, 57309-005. E-mail
14 addresses: ss.albuquerque@gmail.com / emerson.fis.ara@gmail.com.

15

16 ***Corresponding Author**

17 Prof. Pierre Barnabé Escodro, Department of Veterinary Medicine, Federal University of
18 Alagoas, Fazenda São Luiz s/n, Viçosa, Alagoas State, Brazil, 5700-000. E-mail address:
19 pierre.escodro@vicos.ufal.br (PB. Escodro).

20

21 **Abstract**

22 This study proposed a loading capacity equation for urban cart-pulling equids. The research was
23 conducted in two stages: the first developed the equation, and the second applied it by analyzing
24 the zoometric structure of animals already employed in this activity. The equation was
25 formulated by applying Newton's laws of motion, starting from an ideal model that did not
26 consider dissipative forces, and the variables, such as friction force, animal morphological
27 indices and maximum supported load, were subsequently added. Next, the equation was applied
28 using body weight data for 228 pulling equids, including 49 horses (18 males and 31 females)
29 and 179 mules (13 males and 166 females), estimating the mean body weight for each sex in
30 both species. This evaluation also considered variations in terrain friction coefficients on
31 different terrains. The value of 0,0015 was used as the friction coefficient for spherical bearings
32 in the cart axles. The results were subjected to analysis of variance and means testing (Duncan's
33 test at 5% probability) to establish the relationship between the resulting means for male and
34 female horses and mules separately. The maximum load value obtained in these cases was
35 approximately twice the animals' mean live weight. The findings of this study indicate that
36 equations can be applicable and should be validated by additional experiments using alive
37 equids.

38 **Keywords:** *Equus*, Load, Physics, Capacity.

39

40 **1. Introduction**

41 Equid breeding mainly focuses on athletics and recreation, pulling equids are still needed,
42 which, contrary to expectations, are associated with large urban areas in Brazil, where many are
43 present [1]. Many problems are associated with using cart equids in Brazil, often leading the
44 activity to be viewed in a discriminatory manner by most of society. A study conducted by Souza
45 [2] in the city of Rio de Janeiro addresses the need for legally regulating the activity and for
46 providing environmental education and social assistance to the stakeholders involved to reduce
47 harm to the animals due to misuse and lack of driver preparation.

48 Oliveira et al. [3] conducted a similar study in the city of Uberlândia, Minas Gerais state,
49 and indicated that the activity's main problems were that drivers were unprepared and received
50 no assistance and that the pulled load limits were unregulated, a factor that often damaged the
51 animals' health and productive longevity.

52 The striking presence of animal-drawn carts in large Brazilian urban centers has recently
53 led to municipal laws being enacted to adjust the activity to acceptable standards for most of the
54 population. However, these actions almost always address vehicle and driver identification via
55 license plates and drivers' licenses as a possible means to punish drivers involved in traffic
56 accidents. All attempts to establish the loading capacity for cart-pulling animals are empirical
57 and not backed by research. This creates risks for the activity, in the sense that in some cases the
58 regulations can consider a maximum load that underestimates the capacity of the animals and
59 economically makes the work unworkable, or in the opposite sense of overestimating the
60 maximum load, inevitably promoting health risks and welfare of horses and mules using in this
61 work.

62 Equids can be classified according to their suitability for a given task by
63 analyzing existing relationships among animal body measurements [4]. Thus, zoometry
64 studies generate evidence for analyzing the animals' productive suitability, which, for
65 equids, always involves an aspect of the driving power produced. Mariz et al. [5]
66 analyzed cart-pulling equids in the urban area of Arapiraca, Alagoas state-Brazil, and
67 identified that mules (76%) were more prevalent than horses (21%) and asses (3%) and
68 that the estimated weights varied significantly among these groups.

69 Among the many existing zoometric indices, some are useful for identifying
70 suitable pulling equids, such as those listed below, per Astiz [4]. First is the conformation
71 index or Baron's index, which uses the relationship between the square of the animal's
72 thoracic perimeter and the withers height to determine an index that reflects whether the
73 equid is suitable for pulling tasks when the resulting value is greater than or equal to
74 2.116. Another important index for determining productive aptitude is the dactyl-thoracic
75 index, given by the relationship between the shin perimeter and the thoracic perimeter,
76 for which values above 0.108 indicate individuals suited for pulling. Although considered
77 valid in the equestrian environment for productive animal typification, neither of these
78 two indexes can serve as a reference for solving the problem of maximum load supported
79 by cart-pulling equids.

80 Recent studies have attempted to estimate equid loading capacities, either on the animal's
81 backs, as described by Matsuura et al. [6], or in agricultural traction, as described by Spugnoli et
82 al. [7]. In the latter case, equipment was developed for this purpose. It is possible, however, to
83 attempt to formulate an equation using Newton's laws of motion to determine a load capacity
84 index for traction equids. Rooney & Turner [8] started the theoretical study about the mechanics

85 of horses pulling loads, showed that with a draft angle of zero, shafts parallel to the ground,
86 evidencing the horse must only exert a horizontal force to move the load. Hiraga & Sugano
87 [9] conducted a review of the literature of research conducted between 1950 and 1960 in Japan
88 with draft horses, and highlighted results of correlation between the live weight of the animals
89 and the carrying capacity of the animals, regardless of whether they belong to races selected for
90 traction. One of the results showed that ponies of approximately 200 kg could draw up to 1000
91 kg and double their weight during a working day.

92 This study proposed a load capacity equation for pulling equids and testing it
93 theoretically using data by zoometric structure of animals already employed in this activity, to
94 assist with regulating this activity in Brazil by establishing standards that enhance the use of
95 these animals without endangering their welfare.

96

97 **2. Materials and Methods**

98 The research was approved by the Ethics Research Committee on Animal Use (CEUA),
99 Federal University of Alagoas, in Maceió, Brazil (Protocol 0007/12) and performed in two
100 stages:

101 - Developed the load capacity equation for pulling equids, which differed for horses and
102 mules. The equation was formulated by applying Newton's laws of motion, starting from an ideal
103 model that did not consider dissipative forces, and the variables, such as friction force, animal
104 morphological indices and maximum supported load, were subsequently added.

105 - Application of the equations to predict load capacity using body weight data from 228
106 pulling equids from Arapiraca, Alagoas state, Brazil, of which 49 were horses (18 males and 31

107 females) and 179 were mules (13 males and 166 females), in conditions of the Brazilian
108 Northeast region.

109 The study of equid walking gaits considers that equids move in equal time
110 intervals, ensuring that the motion is performed at a constant speed different from zero;
111 thus, the problem can be discussed based on the principles of Newton's second law and
112 the resulting force. In the first moment, the motion has constant speed with acceleration
113 equal to zero. Were considered the friction coefficient of distinct types of terrain,
114 including asphalt (0.01), rough asphalt (0.011), rough cement (0.014), cobblestone (0.02),
115 irregular stones (0.032), compacted gravel (0.045), compacted dirt (0.06), loose gravel
116 (0.08), grass (0.1), loose sand (0.3) and clay (0.4), and the mean friction coefficient of
117 these terrains (0.097). A friction coefficient of 0.0015 was used for the spherical bearings
118 in the cart axles [10,11].

119 In order to allow the calculation of a series of body indexes, which were used to
120 characterize the average productive type found in the equidae population analyzed,
121 several zoomometric measures were taken, whether at the height of the withers (AC),
122 height of croup (GA), body length (CC), croup length (CG), croup width in the ileum
123 (LGil), chest width (LP), chest depth (ProT), thoracic perimeter (PerT) and perimeter of
124 cannon (PerC) [5].

125 By means of the mathematical interrelations drawn between the zoometric
126 measures obtained, a series of corporal indexes was calculated as Body Mass (MC),
127 product of the thoracic perimeter raised to the cube by the constant 80; the Body Index
128 (ICorp), relationship between the product of body length measurement with constant 100
129 and the thoracic perimeter; the Proportionality Index (IProp), dividing the product

130 between the measure of the height of the withers and the constant 100, by the corporal length; the
131 Conformation Index (IConf), relationship between the thoracic perimeter and the height of the
132 withers; the Compass Index (IComp), relationship between body weight and height of withers;
133 the dactylthoracic index (Idt), relationship between the perimeter of the cannon and the thoracic
134 perimeter; Index of Load in Back to Step (ICp), relation between the product of the thoracic
135 perimeter squared with the constant 98 and the height of the withers; Index of Back Load to
136 Gallop (ICg), given by the ratio of the product of the thoracic perimeter squared to the constant
137 56, and the height of the withers. The individuals were classified as longileneus (Body Index
138 superior to 90, work in speed), mediolineus (between 86 and 88, intermediate work) and
139 brevilineus (less than 85, force work) [4,5].

140 The means of the generated equations, which differed between the species due to their
141 variable load-pulling capacities, were statistically analyzed by Duncan's test at 5% probability
142 using the SAS statistical package.

143

144 **3. Results and Discussion**

145 -Development of equation

146

147 The friction force (f) is the sum of the friction force from the bearings (gears) and from
148 the rolling tire (resistance to rolling on the ground). In this case, movement between the gears
149 indicates that this force depends on the dynamic friction coefficient of the bearings. As the tire is
150 not slipping, static friction force provides the limit value that the tire can support when on the
151 verge of slipping. The friction force or rolling resistance that gives the value of the friction force

152 acting on the system is obtained by replacing the static coefficient with the rolling
 153 resistance coefficient.

154 Thus, the system's overall friction coefficient is the sum of the kinetic (μ_k) and
 155 rolling resistance coefficients (μ_r). Since the gear bearings are spherical, μ_k has a value
 156 of 0.0015, whereas the μ_r values depend on the ground friction coefficient.

157 As motion occurs in the horizontal plane, the normal force (N) equals the weight
 158 force (W) due to the load; thus, we have:

$$159 \quad Fca - \mu.M \cdot g = 0$$

160 To find the total mass (M), this term is isolated in the equation:

$$161 \quad M = \frac{Fca}{(\mu_k + \mu_r).g}$$

162 where:

163 M = total mass in kilograms (kg) that the equid can pull by walking at a constant
 164 speed;

165 Fca = force produced by the equid in newtons (N);

166 μ_k = coefficient of kinetic friction between the bearings, dimensionless, whose
 167 value is 0.0015;

168 μ_r = coefficient of rolling resistance friction on the ground, dimensionless,
 169 varying by terrain: smooth asphalt (0.01), rough asphalt (0.011), rough cement (0.014),
 170 cobblestone (0.02), irregular stones (0.032), compacted gravel (0.045), compacted dirt
 171 (0.06), loose gravel (0.08), grass (0.1), loose sand (0.3), clay (0.4) and mean friction
 172 coefficient for all these terrains (0.097) [10/11];

173 g = gravitational acceleration at sea level, given in meters per second squared (m/s^2),
 174 having an approximate constant value of 9.8.

175 The equation varies between horses and mules [12,13] since the inherent tractive force
 176 correlates with the animals' mass, thus generating two distinct correction factors that are applied
 177 as follows:

178 For horses:

$$179 \quad M = \frac{1.88W}{(\mu k + \mu r).g}$$

180 For mules:

$$181 \quad M = \frac{2.115W}{(\mu k + \mu r).g}$$

182 where:

183 W = calculated animal weight, which is the equid's body mass in kilograms (kg).

184 It is important to note that these equations are only valid for the horizontal plane and at
 185 constant walking speed since the speed would vary on any inclined plane, as the weight force in
 186 the direction of motion in this case is not zero.

187

188 -Application of the equations in horses and mules

189 Were used zoometric data for 228 pulling equids from Arapiraca, Alagoas state, Brazil,
 190 of which 49 were horses (18 males and 31 females) and 179 were mules (13 males and 166
 191 females) were used to simulate results using the equation.

192 Analyzing the body indexes (Table 1), it is observed that the horses presented body
 193 indexes with values higher than the mules. According to the results of the body index (ICorp),

194 horses and mules are classified as mediolineus (between 86 and 88, intermediate work),
 195 based on the classification of Astiz [4]. This indicates that all the animals used in the
 196 traction activity in the municipality of Arapiraca do not have adequate body index for this
 197 purpose, demonstrating the importance of an equation such as this being proposed, which
 198 can at least be used to draw a maximum reference load on the coupling.

199 **Table 1**

200 Body indexes calculated in urban traction equidae such as Body Mass (MC), Body Index
 201 (ICorp), Conformation Index (IConf), Compass Index (IComp), Thoracic Dactyl Index (Idt),
 202 Load Index to Step (ICdp) and Gallop Loading Index (ICdg).

	MC (kg)	ICorp	IConf	IComp	Idt	ICdp (kg)	ICdg (kg)
Mules	270±47.9b	86.4±3.8b	1.726±0.14b	2.0±0.31b	0.106±0.007	169±13.72b	96±7.84b
Horses	322±42.3a	86.7±3.02b	1.832±11.04a	2.3±0.21a	0.110±0.007	179±10.82a	102±6.18a
CV	16.68	4.22	7.66	13.63	6.35	7.66	7.66

203 Means followed by different letters in the same column differ statistically (P <0.05) by the Skott-
 204 Knott test. C.V. - coefficient of variation (%).

205

206 Table 2 shows the estimated loading capacity (kg) of horses in Arapiraca,
 207 considering mean live weights for males and females and different terrains for
 208 locomotion.

209 **Table 2**

210 Estimated load capacity (kg) for male and female horses, according to body weight and terrain
 211 type, given by the equation developed for the species.

Terrain type (friction coefficient)	Males (kg)	Females (kg)
Smooth Asphalt (0.01)	5655.1±700.7a	5227±668.6b
Rough Asphalt (0.011)	5202.7±644.7a	4808.8±615.1b
Rough Cement (0.014)	4195.7±519.9a	3878.1±496.1b
Cobblestone (0.02)	3024.8±374.8a	2795.8±357.6b
Irregular Stones (0.032)	1941.3±240.6a	1794.3±229.5b
Compacted Gravel (0.045)	1398.6±173.3a	1292.7±165.4b
Compacted Dirt (0.06)	1057.5±131a	977.4±125b
Loose Gravel (0.08)	798±98.9a	737.6±94.3b
Grass (0.1)	640.7±79.4a	592.2±75.8b
Loose Sand (0.3)	215.7±26.7a	199.4±25.5b
Clay (0.4)	162±20.1a	149.7±19.2b
Mean Terrain Coefficient (0.097)	660.2±81.8a	610.3±78.1b

212 Means followed by different letters differ significantly per Duncan's test at 5% probability.

213

214 The mean body weight of the male horses was 339±26.3 kg and of the female horses was
215 313.3±43.9 kg, which led to the standardized response observed in the data where the loading
216 capacity of the stallions was always greater than that of the mares, as the live animal weight is
217 the equation element that reflects each individual's working capacity. Mares are preferred
218 because they are also used for breeding, as with the mares, and are calmer, which facilitates
219 traction work. This temperament is also seen in castrated horses, but castration is costly, and the
220 animals cannot work for some time after the procedure. Another reason that owners report

221 preferring females is that females do not have to stop pulling the carts to urinate, thus
222 making it difficult when males require unscheduled stops in high traffic locations.

223 The animal's body mass classifies them as small or hypometric equids since they
224 are below 350 kg [4]. Hypometric animals have also been described in other studies, such
225 as by Paz et al. [14], who observed that the mean weight of traction horses in the city of
226 Pelotas, Rio Grande do Sul state, was 321 kg, a value close to that of the horses in this
227 study. These scarce data show that the type of horses used to pull carts in Arapiraca is
228 similar to that in other localities.

229 In evaluating the loading-pulling capacity of these animals according to the
230 supporting terrain type, it is interesting that the values vary extensively, ranging from
231 loads that are much greater than the animal's live weight, as with traction on smooth
232 asphalt, for which the value is up to 16-fold, to loads that are much smaller than the
233 animal's live weight, as with the pulling capacity on clay, for which the value is less than
234 half the animals' live body weight.

235 These situations are produced by the physical aspects of the cart pulling process,
236 where the major determinant of the maximum weight supported is given by the capacity
237 of the pulling agent (the animal) to remove the vehicle from the state of inertia. Thus, in
238 terrain conditions where the friction force, which is contrary to the traction movement, is
239 small, this capacity increases greatly, while the inverse condition occurs when this
240 friction force is large.

241 Table 3 presents the estimated loading capacity (kg) data for mules in Arapiraca,
242 Alagoas state, Brazil, considering mean live weights for males and females and different
243 terrains for locomotion.

244 **Table 3**

245 Estimated loading capacity (kg) for male and female mules, according to body weight and terrain
 246 type, given by the equation developed for the species.

Terrain Type (friction coefficient)	Males (kg)	Females (kg)
Smooth Asphalt (0.01)	4419±697.7b	5120.9±895.5a
Rough Asphalt (0.011)	4065.5±641.9b	4711.2±823.9a
Rough Cement (0.014)	3278.6±517.7b	3799.3±664.4a
Cobblestone (0.02)	2363.6±373.2b	2739.1±479a
Irregular stones (0.032)	1517±239.5b	1757.9±307.4a
Compacted Gravel (0.045)	1092.9±172.6b	1266.4±221.5a
Compacted Dirt (0.06)	826.3±130.5b	957.6±167.5a
Loose Gravel (0.08)	623.5±98.4b	722.6±126.4a
Grass (0.1)	500.7±79.1b	580.2±101.5a
Loose Sand (0.3)	168.6±26.6b	195.3±34.2a
Clay (0.4)	126.6±20b	146.7±25.7a
Mean Terrain Coefficient (0.097)	515.9±81.5b	597.9±104.6a

247 Means followed by different letters differ significantly per Duncan's test at 5% probability.

248

249 The mean body weight of the male mules was 235.5±26.4 kg and of the females was
 250 272.9±48.6 kg, which also led to the standardized response observed in the data where the
 251 loading capacity of the female mules was always higher than that of the males, the inverse
 252 situation to that for the horses. Female mules are preferred because they are calmer, which
 253 facilitates traction work.

254 In Arapiraca, the selection of female mules is also more judicious than that of
255 males, as evidenced by the greater body weight of females than males. Based on mean
256 live weight, the mules studied were also small or hypometric, as they weighed less than
257 350 kg [4].

258 Assessment of the load-pulling capacity of the mules according to supporting
259 terrain shows a pattern similar to that in Table 3 since the terrain friction coefficients are
260 the same.

261 Notably, in both tables, the load values obtained considering the mean terrain
262 friction coefficient are important since they represent a hypothetical average situation that
263 theoretically would give the animals satisfactory working conditions when facing diverse
264 terrains throughout the day. The maximum load value obtained in these cases is
265 approximately twice the mean live weight of the animals, which generates a very
266 comfortable limit, as the animals are not bearing all this weight force on their backs.

267 **4. Conclusion**

268 The equations may be applicable and should be verified by additional
269 physiological and biochemical tests considering the mean terrain coefficient, as well as
270 variables such as number of hours worked and situations with sloped terrain.

271

272 **Acknowledgements**

273 - To the Institute of Physics- Federal University of Alagoas for the support in the development of
274 the equations for analysis of load capacity.

275 - The American Journal Experts for the correction and version of the text in the English
276 language.

277

278 **Funding**

279 This research did not receive any specific grant from funding agencies in the public, commercial,
280 or not-for-profit sectors.

281

282 **Conflict of Interest**

283 Conflict of interest none.

284

285 **Author Contributors**

286 Tobyas Maia de Albuquerque Mariz, Pierre Barnabé Escodro, Carolyny Batista Lima, Jéssyka
287 Emmanuely Silva dos Santos and Andrezza Caroline Aragão da Silva: Experimental execution
288 and adequacy of equations

289 Emerson de Lima and Samuel Albuquerque: Proposition and development of the equations.

290

291 **References**

292 [1] Escodro PB, Silva TJF, Mariz TMA, Lima ES. Estudo da realidade e propostas de ações
293 transdisciplinares para equídeos de tração carroceiros de Maceió-Alagoas. Rev Bras
294 Direito Anim 2012;7:97–115.

295 [2] Souza MFA. Implicações para o bem-estar de equinos usados para tração de veículos.
296 Rev Bras Direito Anim 2006;1:1–6.

297 [3] Oliveira L, Marques R, Nunes C, Cunha A. Carroceiros e equídeos de tração: um
298 problema socioambiental. Caminhos Geogr 2007;8:204–16.

- 299 [4] Astiz CS. Valoración morfológica de los animales domésticos. Ministerio de Medio
300 Ambiente y Medio Rural y Marino-España; 2009.
- 301 [5] Mariz TMA, Escodro PB, Dittrich JR, Neto MS, Lima CB, Ribeiro JS. Padrão
302 biométrico, medidas de atrelagem e índice de carga de equideos de tração urbana do
303 município de Arapiraca, Alagoas. Arch Vet Sci 2014;19:1-8.
- 304 [6] Matsuura A, Irimajiri M, Matsuzaki K, Hiraguri Y, Nakanowatari T, Yamazaki A, et al.
305 Method for estimating maximum permissible load weight for Japanese native horses
306 using accelerometer-based gait analysis. Anim Sci J 2013;84:75-81.
- 307 [7] Spugnoli P, Parenti A, Masella P, Melani E. Test of an animal drawn field implement
308 cart. J Ag Eng. - Riv Ing Agr 2008;2:1-5.
- 309 [8] Rooney JR, Turner LW. The mechanics of horses pulling loads. Journal of Equine
310 Veterinary Science 1985;5(6): 355-359.
- 311 [9] Hiraga A, Sugano S. Studies on the exercise physiology of draft horses performed in
312 Japan during the 1950s and 1960s. Journal of Equine Science 2017; 28(1): 1-12.
- 313 [10] Blau, PJ. Friction Science and Technology: From concepts to applications. 2nd ed. New
314 York: CRC Press; 2009.
- 315 [11] Halliday D, Resnick R, Walker J. Fundamentos de física-mecânica. 8th ed. Rio de
316 Janeiro: Editora LTC; 2009.
- 317 [12] Goe MR, McDowell RE. Animal traction: guidelines for utilization. Cornell International
318 Agriculture Mimeo, p. 37-39. 1980.
- 319 [13] Beretta CC. Tração animal na agricultura. São Paulo: Nobel; 1988.

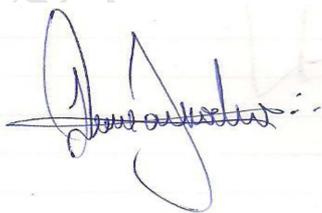
- 320 [14] Paz CFR, Paganela JC, Oliveira DP, Feijó LS, Nogueira CEW. Padrão biométrico dos
321 cavalos de tração da cidade de pelotas no rio grande do sul. Ciênc Anim Bras
322 2013;14:159–63.
323

HIGHLIGHTS

Manuscript title: Equation for Predicting the Load-Pulling Capacity of Traction Equids

The paper intitled **Equation for Predicting the Load-Pulling Capacity of Traction Equids** seeks to fill a gap with regard to the load capacity for traction equids, being able to be enumerated as highlights of the research:

- Development of a physical equation to calculate the load capacity taking into account the body mass of the animal, structural characteristics of the cart and soil type.
- Application of the equation in 288 equids, being 179 mules, of traction activity for human subsistence in the Alagoas state, Brazil.
- The research makes potential future projects in the physiology of the exercise of traction animals and animal welfare.
- Possibility of establishing regulatory norms for load capacity of the urban traction equids in developing countries, since the number of animals in the cities used for the transportation of people and freight is still high, under conditions of mistreatment.



Pierre Barnabé Escodro